Buck Converter - DC-DC

3 MHz, 600 mA

The NCP1522B step−down DC−DC converter is a monolithic integrated circuit optimized for portable applications powered from one cell Li−Ion or three cell Alkaline/NiCd/NiMH batteries. The part, available in adjustable output voltage versions ranging from 0.9 V to 3.3 V, is able to deliver up to 600 mA. It uses synchronous rectification to increase efficiency and reduce external part count. The device also has a built–in 3 MHz (nominal) oscillator which reduces component size by allowing smaller inductors and capacitors. Automatic switching PWM/PFM mode offers improved system efficiency.

Additional features include integrated soft−start, cycle−by−cycle current limiting and thermal shutdown protection. The NCP1522B is available in a space saving, low profile TSOP5 and UDFN6 packages.

Features

- Up to 93% Efficiency
- Allow Use of Small External Components
- Source up to 600 mA
- 3 MHz Switching Frequency
- Adjustable Output Voltage from 0.9 V to 3.3 V
- Synchronous Rectification for Higher Efficiency
- 2.7 V to 5.5 V Input Voltage Range
- Low Ouiescent Current
- \bullet Shutdown Current Consumption of 0.3 µA
- Thermal Limit Protection
- Short Circuit Protection
- All Pins are Fully ESD Protected
- These are Pb−Free Devices

Typical Applications

- Cellular Phones, Smart Phones and PDAs
- Digital Still/Video Cameras
- MP3 Players and Portable Audio Systems
- Wireless and DSL Modems
- Portable Equipment
- USB Powered Devices

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ORDERING INFORMATION

†For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specification Brochure, BRD8011/D.

NCP1522B

PIN FUNCTION DESCRIPTION

PIN CONNECTIONS

Figure 5. Pin Connections − TSOP−5 Figure 6. Pin Connections − UDFN6

MAXIMUM RATINGS

Stresses exceeding Maximum Ratings may damage the device. Maximum Ratings are stress ratings only. Functional operation above the Recommended Operating Conditions is not implied. Extended exposure to stresses above the Recommended Operating Conditions may affect device reliability.

1. Maximum electrical ratings are defined as those values beyond which damage to the device may occur at $T_A = 25^{\circ}C$.

2. According to JEDEC standard JESD22−A108B.

- 3. This device series contains ESD protection and exceeds the following tests:
- Human Body Model (HBM) per JEDEC standard: JESD22−A114.

Machine Model (MM) per JEDEC standard: JESD22−A115.

4. Latchup current maximum rating per JEDEC standard: JESD78.

5. JEDEC Standard: J−STD−020A.

NCP1522B

6. The overall output voltage tolerance depends upon the accuracy of the external resistor (R1, R2).

7. For V_{OUT} = 0.9 V, maximum input voltage do not exceed 5.2 V.

TABLE OF GRAPHS

NCP1522B

DC/DC OPERATION DESCRIPTION

Detailed Description

The NCP1522B uses a constant frequency, voltage mode step−down architecture. Both the main (P−Channel MOSFET) and synchronous (N−Channel MOSFET) switches are internal.

The output voltage is set by an external resistor divider in the range of 0.9 V to 3.3 V and can source at least 600 mA.

The NCP1522B works with two modes of operation; PWM/PFM depending on the current required. In PWM mode, the device can supply voltage with a tolerance of \pm 3% and 90% efficiency or better. Lighter load currents cause the device to automatically switch into PFM mode to reduce current consumption and extended battery life.

Additional features include soft−start, undervoltage protection, current overload protection, and thermal shutdown protection. As shown in Figure [1](#page-0-0), only six external components are required. The part uses an internal reference voltage of 0.6 V. It is recommended to keep NCP1522B in shutdown mode until the input voltage is 2.7 V or higher.

PWM Operating Mode

In this mode, the output voltage of the device is regulated by modulating the on−time pulse width of the main switch Q1 at a fixed 3 MHz frequency.

The switching of the PMOS Q1 is controlled by a flip−flop driven by the internal oscillator and a comparator that compares the error signal from an error amplifier with the sum of the sensed current signal and compensation ramp.

The driver switches ON and OFF the upper side transistor (Q1) and switches the lower side transistor in either ON state or in current source mode.

At the beginning of each cycle, the main switch Q1 is turned ON by the rising edge of the internal oscillator clock. The inductor current ramps up until the sum of the current sense signal and compensation ramp becomes higher than the error amplifier's voltage. Once this has occurred, the PWM comparator resets the flip−flop, Q1 is turned OFF while the synchronous switch Q2 is turned in its current source mode. Q2 replaces the external Schottky diode to reduce the conduction loss and improve the efficiency. To avoid overall power loss, a certain amount of dead time is introduced to ensure Q1 is completely turned OFF before Q2 is being turned ON.

PFM Operating Mode

Under light load conditions, the NCP1522B enters in low current PFM mode operation to reduce power consumption. The output regulation is implemented by pulse frequency modulation. If the output voltage drops below the threshold of PFM comparator, a new cycle will be initiated by the PFM comparator to turn on the switch Q1. Q1 remains ON during the minimum on time of the structure while Q2 is in its current source mode. The peak inductor current depends upon the drop between input and output voltage. After a short dead time delay where Q1 is switched OFF, Q2 is turned in its ON state. The negative current detector will detect when the inductor current drops below zero and sends the signal to turn Q2 to current source mode to prevent a too large deregulation of the output voltage. When the output voltage falls below the threshold of the PFM comparator, a new cycle starts immediately.

Figure 28. PFM Switching Waveforms (V_{IN} = 3.6 V, V_{OUT} = 1.2 V, I_{OUT} = 0 mA, Temp = 25°C)

Soft−Start

The NCP1522B uses soft−start to limit the inrush current when the device is initially powered up or enabled. Soft−start is implemented by gradually increasing the reference voltage until it reaches the full reference voltage. During startup, a pulsed current source charges the internal soft−start capacitor to provide gradually increasing reference voltage. When the voltage across the capacitor ramps up to the nominal reference voltage, the pulsed current source will be switched off and the reference voltage will switch to the regular reference voltage.

Cycle−by−Cycle Current Limitation

From the block diagram, an $I_{\text{I} \text{I} \text{M}}$ comparator is used to realize cycle−by−cycle current limit protection. The comparator compares the LX pin voltage with the reference voltage, which is biased by a constant current. If the inductor current reaches the limit, the I_{LIM} comparator detects the LX voltage falling below the reference voltage and releases the signal to turn off the switch Q1. The cycle−by−cycle current limit is set at 1200 mA (nom).

Low Dropout Operation

The NCP1522B offers a low input to output voltage difference. The NCP1522B can operate at 100% duty cycle. In this mode the PMOS (Q1) remains completely on.

The minimum input voltage to maintain regulation can be calculated as:

 $VIN(min) = VOUT(max)$ (eq. 1) $+$ (IOUT \times (RDS(ON) $+$ RINDUCTOR))

- VOUT: Output Voltage (Volts)
- IOUT: Max Output Current
- $R_{DS(ON)} = P-Channel Switch R_{DS(ON)}$
- R_{INDUCTOR}: Inductor Resistance (DCR)

Undervoltage Lockout

The input voltage V_{IN} must reach 2.4 V (typ) before the NCP1522B enables the DC/DC converter output to begin the start up sequence (see Soft−Start section). The UVLO threshold hysteresis is typically 100 mV.

Shutdown Mode

Forcing this pin to a voltage below 0.4 V will shut down the IC. In shutdown mode, the internal reference, oscillator and most of the control circuitries are turned off. Therefore, the typical current consumption will be $0.3 \mu A$ (typical value). Applying a voltage above 1.2 V to EN pin will enable the device for normal operation. The typical threshold is around 0.7 V. The device will go through soft−start to normal operation.

Thermal Shutdown

Internal Thermal Shutdown circuitry is provided to protect the integrated circuit in the event that the maximum junction temperature is exceeded. If the junction temperature exceeds 160°C, the device shuts down. In this mode switch Q1 and Q2 and the control circuits are all turned off. The device restarts in soft−start after the temperature drops below 135°C. This feature is provided to prevent catastrophic failures from accidental device overheating, and it is not intended as a substitute for proper heatsinking.

Short Circuit Protection

When the output is shorted to ground, the device limits the inductor current. The duty−cycle is minimum and the consumption on the input line is 300 mA (Typ). When the short circuit condition is removed, the device returns to the normal mode of operation.

APPLICATION INFORMATION

Output Voltage Selection

The output voltage is programmed through an external resistor divider connected from V_{OUT} to FB then to GND. For low power consumption and noise immunity, the resistor from FB to GND (R2) should be in the [100 k–600 k] range. If R2 is 200 k given the V_{FB} is 0.6 V, the current through the divider will be $3.0 \mu A$.

The formula below gives the value of V_{OUT} , given the desired R1 and the R1 value:

$$
VOUT = VFB \times (1 + \frac{R1}{R2})
$$
 (eq. 2)

- V_{OUT} : Output Voltage (Volts)
- V_{FB} : Feedback Voltage = 0.6 V
- R1: Feedback Resistor from V_{OUT} to FB
- R2: Feedback Resistor from FB to GND

Input Capacitor Selection

In PWM operating mode, the input current is pulsating with a large switching noise. Using an input bypass capacitor can reduce the peak current transients drawn from the the state of the s

input supply source, thereby reducing switching noise significantly. The capacitance needed for the input bypass capacitor depends on the source impedance of the input supply.

The maximum RMS current occurs at 50% duty cycle with maximum output current, which is $I_{out,max}/2$.

For NCP1522B, a low profile ceramic capacitor of 4.7μ F should be used for most of the cases. For effective bypass results, the input capacitor should be placed as close as possible to the V_{IN} pin.

Table 1. List of Input Capacitors

Output L−C Filter Design Considerations

The NCP1522B operates at 3 MHz frequency and uses voltage mode architecture. The correct selection of the output filter ensures good stability and fast transient response.

Due to the nature of the buck converter, the output L−C filter must be selected to work with internal compensation. For NCP1522B, the internal compensation is internally fixed and it is optimized for an output filter of $L = 2.2 \mu H$ and $C_{\text{OUT}} = 4.7 \mu F$.

The corner frequency is given by:

$$
f_{C} = \frac{1}{2\pi\sqrt{L \times C_{OUT}}} = \frac{1}{2\pi\sqrt{2.2 \ \mu H \times 4.7 \ \mu F}} = 49 \ \text{kHz}
$$
\n
$$
\text{(eq. 3)}
$$

The device is intended to operate with inductance value of $2.2 \mu H$.

If the corner frequency is moved, it is recommended to check the loop stability depending on the accepted output ripple voltage and the required output curret. Take care to check the loop stability. The phase margin is usually higher than 45°.

Table 2. L−C Filter Example

Inductor Selection

The inductor parameters directly related to device performances are saturation current and DC resistance and inductance value. The inductor ripple current (ΔI_L) decreases with higher inductance:

$$
\Delta I_L = \frac{VOUT}{L \times fSW} \bigg(1 - \frac{VOUT}{VIN} \bigg) \hspace{1.0cm} \text{(eq. 4)}
$$

- ΔI_L : Peak to Peak Inductor Ripple Current
- L: Inductor Value
- $f_{SW:}$ Switching Frequency

The saturation current of the inductor should be rated higher than the maximum load current plus half the ripple current:

$$
I_{L(MAX)} = I_{O(MAX)} + \frac{\Delta I_L}{2}
$$
 (eq. 5)

- $\Delta I_{L(MAX)}$: Maximum Inductor Current
- \bullet $\Delta I_{O(MAX)}$: Maximum Output Current

The inductor's resistance will factor into the overall efficiency of the converter. For best performance, the DC resistance should be less than 0.3 Ω for good efficiency.

Table 3. LIST OFINDUCTORS

Output Capacitor Selection

Selecting the proper output capacitor is based on the desired output ripple voltage. Ceramic capacitors with low ESR values will have the lowest output ripple voltage and are strongly recommended. The output capacitor requires an X7R dielectric.

The output ripple voltage in PWM mode is given by:

$$
\Delta V_{\text{OUT}} = \Delta I_{\text{L}} \times \left(\frac{1}{4 \times f_{\text{SW}} \times C_{\text{OUT}}} + \text{ESR} \right) \quad \text{(eq. 6)}
$$

- \bullet ΔV_{OUT} : Output Voltage Ripple in PWM Mode
- ΔI_{L} : Peak to Peak Inductor Ripple Current
- f_{SW}: Switching Frequency
- COUT: Output Capacitor
- ESR: Output Capacitor Serial Resistor

Table 4. LIST OF OUTPUT CAPACITORS

Feed−Forward Capacitor Selection

The feed−forward capacitor sets the feedback loop response and is critical to obtain good loop stability.

Given that the compensation is internally fixed, an 18 pF or higher ceramic capacitor is needed. Choose a small ceramic capacitor X7R dielectric.

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